

Amendments to the Specification:

Please replace the paragraph beginning at page 16, line 5, with the following rewritten paragraph:

-- Fig. 1 is a view showing an X-ray diffraction chart of an embodiment of a carrier core material of the present invention, in which the high-melting point oxide ($M^H O$) appears as a peak of an element that is not ferrite- ferrite; and --

Please replace the paragraph beginning at page 21, line 4, with the following rewritten paragraph:

-- By allowing the high-melting point oxide ($M^H O$) to be independently present in the ferrite component without forming a solid solution as described above, the high-melting point oxide ($M^H O$) has a function of depressing electrical conductivity among crystals of the ferrite, and there can be prepared a carrier core material capable of forming a coated carrier which is free from leakage of electric charge even in a high electric field in spite of the fact that it has high magnetization. Especially when the high-melting point oxide ($M^H O$) is allowed to be present inside the particle of the carrier core material in a concentration higher than that in the vicinity of the particle surface of the carrier core material, a phenomenon of leakage of electric charge in a high electric field can be inhibited by the contribution of the resistance inside the particle, and there can be obtained a carrier core material suitable for preparing a coated carrier having higher magnetization and free from leakage of electric charge in a high electric field. It is important that the high-melting point oxide ($M^H O$) that is present independently as described above is contained together with the low-melting point oxide ($M^L O$), and by the control of the content of the high-melting point oxide ($M^H O$), it becomes possible to disperse the high-melting point oxide ($M^H O$) inside the particle and to control the concentration thereof in the vicinity of the particle surface. Consequently, the carrier core material of the invention becomes suitable for forming a coated carrier having high magnetization and rarely suffering leakage of electric charge over a wide range of electric field from low electric field to high electric field even if the resin coating is abraded by the printing impression. --

Please replace the paragraph beginning at page 30, line 8, with the following rewritten paragraph:

-- The magnetization (M_s) of the carrier core material of the invention at 1000 ($10^3/4\pi \cdot A/m$) (1000 oersted), as measured in the above-mentioned manner, is in the range of

usually 40 to 100 Am²/kg (40 to 100 emu/g), preferably 50 to 95 Am²/kg (50 to 95 emu/g), more preferably 65 to 95 Am²/kg (65 to 95 emu/g). The residual magnetization (Mr) of the carrier core material at 1000 (10³/4π·A/m) (1000 oersted) is usually not more than 20 Am²/kg (20 emu/g), preferably not more than 15 Am²/kg (15 emu/g), particularly preferably not more than 5 Am²/kg (5 emu/g). The coercive force (Hc) of the carrier core material is usually not more than 50 (10³/4π·A/m) (50 oersted), preferably not more than 30 (10³/4π·A/m) (30 oersted), particularly preferably not more than 15 (10³/4π·A/m) (15 oersted). If the magnetization is ~~lower than~~ lower than the lower limit of the above range, carrier adhesion is liable to take place. If the magnetization is higher than the upper limit of the above range, a head of a magnetic brush formed becomes hard. As a result, brush streaks are liable to be produced, and it becomes difficult to form an image of high quality. If the residual magnetization or the coercive force is too high, the developing agent has poor fluidity, and rise of frictional charging between the coated carrier and the toner becomes bad to easily bring about a phenomenon of toner fly or fog. --

Please replace the paragraph beginning at page 45, line 14, with the following rewritten paragraph:

-- The two-component developing agent of the present invention comprises the above-described coated carrier and toner particles. The toner particles for use in the invention include ~~grinded~~ ground toner particles prepared by grinding and polymerized toner particles prepared by polymerization. In the present invention, toner particles obtained by any of those processes are employable. --

Please replace the paragraph beginning at page 45, line 22, with the following rewritten paragraph:

-- The ~~grinded~~ ground toner particles can be obtained by, for example, a process comprising sufficiently mixing a binding resin, a charging controlling agent and a colorant by a mixing machine such as a Henschel mixer, melt kneading the mixture by a twin-screw extruder or the like, then cooling, grinding, classifying, adding external additives and mixing them by a mixer or the like. --

Please replace the paragraph beginning at page 52, line 5, with the following rewritten paragraph:

-- The average particle diameter of the toner particles prepared as above is in the range of 3 to 15 μm, preferably 5 to 10 μm. The polymerized toner particles have higher

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particle uniformity than the ~~grinded~~ ground toner particles. If the average particle diameter of the toner particles is less than 3 μm , charging ability is lowered, and fog or toner fly is liable to occur. If the average particle diameter of the toner particles exceeds 15 μm , image quality may be deteriorated. --